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EDITION OF I NOV 68 IS OBSOLETE

UNCLASSIFIED

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probably Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE 1 INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM NANTICOKE CREEK WATERSHED PROTECTION PROJECT DAM SITE No. 9E I.D. No. NY 575 (#85D-3646) SUSQUEHANNA RIVER BASIN BROOME COUNTY, NEW YORK

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DRAWINGS

PHASE 1 REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Nanticoke Creek Watershed Protection Project Dam Site No. 9E

I.D. No. NY 575 (#85D-3646)

State Located:

New York

County Located:

Broome

Watershed:

Stream:

Unnamed tributary of Nanticoke Creek

Susquehanna River Basin

Date of Inspection:

November 8, 1978

ASSESSMENT

The Nanticoke Creek Watershed Protection Project, Dam Site No. 9E, is a floodwater retarding structure. Examination of available documents and a visual inspection of the dam did not reveal conditions which are considered to be unsafe.

The total discharge capability of the spillway is adequate for the Probable Maximum Flood (PMF).

George Koch

Chief, Dam Safety Section New York State Department of Environmental Conservation

Goorge Koch

NY License No. 45937

Approved By:

Col. Clark H. Benn

New York District Engineer

17 May 17

Date:



NANTICOKE CREEK SITE No. 9E OVERVIEW

PHASE 1 INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
NANTICOKE CREEK WATERSHED PROTECTION PROJECT
DAM SITE No. 9E
I.D. No. NY 575
(#85D-3646)
SUSQUEHANNA RIVER BASIN
BROOME COUNTY, NEW YORK

SECTION 1: PROJECT INFORMATION

1.1 GENERAL

a. Authority

The Phase 1 Inspection reported herein was authorized by the Department of the Army, New York District, Corps of Engineers, to fulfill the requirements of the National Dam Inspection Act, Public Law 92-367.

b. Purpose of Inspection

This inspection was conducted to evaluate the existing conditions of the dam, to identify deficiencies and hazardous conditions, to determine if these deficiencies constitute hazards to life and property, and to recommend remedial measures where required.

1.2 DESCRIPTION OF PROJECT

a. Description of the Dam and Appurtenant Structures
The Nanticoke Creek Watershed Protection Project Dam No. 9E consists of
an earth dam with a principal spillway pipe passing through the embankment and two emergency spillways on the southern end of the dam.

The dam consists of two compacted earth, zoned embankments. The northern embankment is 42 feet high, has a crest length of 520 feet and a crest width of 15 feet. The southern embankment section is 15 feet high, has a crest length of 295 feet and a crest width of 15 feet. The upstream slopes are 1 vertical on 3 horizontal and the downstream slopes are 1 vertical on 2 1/2 horizontal. The crest and exposed slopes are grass covered. An earth cutoff trench of varying depth and width keys both embankments into the foundation soils.

The principal spillway consists of a two stage reinforced concrete drop inlet structure, a 36 inch diameter reinforced concrete pipe with anti-seepage collars, and an impact basin to dissipate energy at the outlet end of the conduit. A reservoir drain consisting of a 12 inch corrugated metal pipe extends from the upstream toe of the embankment to the base of the principal spillway riser. A vertical slide gate mechanism mounted along the inside of the riser controls the flow through the reservoir drain. The emergency spillways are two grass lined channels each 150 feet wide, located in earth cuts on the southeastern end of the dam.

An internal drainage system consisting of a gravel and sand drain fill with perforated 8 inch diameter corrugated metal collector pipes is located at the base of the embankment near the downstream toe. Seepage is collected and conducted through this drain and outleted into the impact basin.

b. Location

Dam No. 9E of the Nanticoke Creek Project is located on an unnamed tributary of the Nanticoke Creek, approximately 1.5 miles north of the Village of Nanticoke. The site is off Cadwell Hill Road in the Town of Nanticoke, New York.

c. Size Classification

This dam is 42 feet high and is classified as an "intermediate" size dam (between 40 and 100 feet high).

d. Hazard Classification

The dam is classified in the "high" hazard category because of the presence of several homes and the Village of Nanticoke downstream of the dam.

e. Ownership

This dam is owned by the County of Broome, New York.

f. Purpose of Dam

This dam is a floodwater retarding structure.

g. Design and Construction History

This dam was designed by the U.S. Department of Agriculture, Soil Conservation Service (SCS). Construction of the dam was completed in 1967. The SCS Office for Broome County, located at the Broome County Airport, has a design folder containing hydrologic, hydraulic, and structural design information, and the as-built plans and documents. These as-built plans were included in the Appendix G.

h. Normal Operating Procedures

Normal flows are discharged through the principle spillway. This structure has sufficient capacity to store and discharge a 100 year flood without flow occuring in the emergency spillway. For storms greater than the 100 year flood, flow will discharge through the emergency spillway.

1.3 PERTINENT DATA

a.	Drainage Area (acres)	1827
ь.	Discharge at Dam (cfs)	
	Principle Spillway at Maximum High Water	165
	Principle Spillway at Emergency Spillway Crest Elevation	156
	Reservoir Drain at Principle Spillway Crest El.	14
	Maximum Known Flood	152
	Emergency Spillway at Maximum High Water	11754
c.	Elevation (USGS datum)	
	Top of Dam	1191.8
	Emergency Spillway Crest (Auziliary Spillway)	1186.7
	Principle Spillway Crest (Service Spillway)	1176.7
	Invert of Reservoir Drain Inlet	1153.0

d.	Reservoir (acres) Surface area at Top of Dam Surface area at Crest of Emergency Spillway Surface area at Crest of Principle Spillway	41.0 32.2 16.2
e.	Storage Capacity (acre-feet) Top of Dam Emergency Spillway Crest Principle Spillway Crest	538 353 120
f.	Dam Embankment Type: A two zoned compacted earth fill in two sections with an earth keyed cutoff trench under each section	
	Embankment Length (ft.) Northern Embankment Section Southeastern Embankment Section	520 295
		cal on 3 horizontal cal on 2.5 horizontal
	Crest Elevation (USGS datum) Both Embankments	1191.8
	Crest Width (ft.) Both Embankments	15
g.	Principal Spillway (Service) Type: Uncontrolled, reinforced concrete two stage drop inlet (3x9 ft.) rising 26.2 feet; 36 inch reinforced concrete pressure conduit 207.58 feet long; concrete impact basin	rced
	Length (ft.) Weir	18
	Emergency Spillway (Auxiliary) Type: Two grass-lined channels having trapezoidal cross sections	s.
	Bottom Width(ft.) Northwestern Channel Southeastern Channel	150 150
	Side Slopes: Both Channels (V : H) Length of level section (in profile) (ft.) Both Channels Exit Slope: Both Channels	1 on 3 30 .028

h. Reservoir Drain

Type:

12 inch diameter corrugated metal pipe with a reinforced concrete inlet.

Control:

Mechanically operated vertical slide gate mounted along the inside of the

principal spillway riser.

SECTION 2: ENGINEERING DATA

2.1 DESIGN

a. Geology

The Nanticoke Creek Watershed Project Dam No. 9E is located in the "Glacitated Allegheny Plateau" physiographic province of New York State. Bedrock underlying the site is mapped as Cashaqua Shale of the Upper Devonian Age. This rock was formed approximately 400 million years ago.

Glacial ice was instrumental in smoothing the topography of the area. The present surficial deposits have resulted primarily from glaciations during the Cenozoic Era, the last of which was the Wisconson glaciation, approximately 11,000 years ago. Glacial deposits such as outwash plains and eskers are major features of the landscape in parts of this region.

b. Subsurface Investigations

A subsurface investigation program was conducted by the Soil Conservation Service in 1965. This program consisted of 17 test pits. The maximum depth of the explorations was 12 feet. Applicable subsurface information is included in Appendix G.

In general, the subsurface conditions on both abutments consist of a thin layer of topsoil underlain by glacial till. In the floodplain, the topsoil layer is underlain by a layer of relatively clean gravel, four to six feet thick. The glacial till is beneath this layer. The cutoff trench was designed to impede seepage through this layer of gravel. Bedrock was not encountered in the exploration program.

c. Embankment and Appurtenant Structures

The dam was designed by the Soil Conservation Service who prepared a design report. Fifteen drawings, several of which have been included in Appendix G, were prepared for the construction of the dam.

The embankment has two zones. Zone 1 is a longitudinal drainage blanket under the downstream slope of the dam, constructed using the clean gravel removed from the cutoff trench excavation. Zone 2 is the relatively impervious glacial till which forms the major portion of both embankments.

2.2 CONSTRUCTION RECORDS

Complete as-built contract plans and documents are available from the SCS Office in Broome County. No major construction changes were made on this job. The as-built plans are included in the Appendix of this report.

2.3 OPERATION RECORD

Since the dam is an uncontrolled, floodwater retarding structure, no operating records are maintained regarding water levels. However, during periods of heavy rainfall, SCS personnel do monitor reservoir levels.

2.4 EVALUATION OF DATA

The data presented in this report has been compiled from information obtained from the Soil Conservation Service as well as the New York State Department of Environmental Conservation files. It appears to be adequate and reliable for the purpose of the Phase 1 Inspection.

SECTION 3: VISUAL INSPECTION

3.1 FINDINGS

a. General

Visual inspection of Dam Site No. 9E was conducted on November 8, 1978. The weather was clear the the temperature was around 50°F. The water surface was several inches above the invert of the low stage inlet on the riser. There was a small flow from the principal spillway pipe spilling into the impact basin.

b. Embankment

The earth embankment showed no signs of distress. The vertical and horizontal alignment of the crest of both embankments appeared to be satisfactory, with no visible surface cracks appearing on the crest or embankment slopes. There were no areas of serious sloughing or subsidence noted. Some minor sloughing was observed on the upstream slope in the range of fluctuation of the water surface level.

Inspection of the downstream face did not reveal any signs of seepage. The collection pipes from theinternal drainage system were dry. There were rock lined trenches to collect surface runoff along the intersection of the downstream toe of the slope with each abutment on the northern embankment section.

No undesirable vegetative growth of animal penetrations into the slopes were observed. However, on the date of the inspection, the grass on the embankments had not been moved.

c. Principal Spillway

The principal spillway consists of the vertical drop inlet structure, a reinforced concrete pressure pipe through the embankment, an impact basin and an outlet channel. All of these components were in satisfactory condition. There was a small gap around the principal spillway pipe at its joint with the headwall of the impact basin.

d. Emergency Spillway

Two grass lined emergency spillways in earth cut sections are located beyond the southern end of the embankment. The spillway had been mowed and appeared to be in satisfactory condition. A small portion had not been mowed because of several logs which had been deposited in the channel.

e. Drain

The reservoir drain conduit and slide gate may be used to lower the reservoir when the pool level is below the principal spillway crest. The slide gate is located within a pipe sleeve which extends to the top of the riser.

f. Downstream Channel

The outlet channel beyond the end of the impact basin was in satisfactory condition. No severe side-slope erosion or debris obstructions were in evidence.

g. Reservoir
There were no signs of soil instability in the reservoir area.

3.2

 $\frac{\text{EVALUATION OF OBSERVATIONS}}{\text{Visual observations did not reveal any problems which would adversely}}$ affect the safety of the dam.

SECTION 4: OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURES

The normal water surface elevation is approximately at the low stage inlet elevation. Downstream flows are limited by the capacity of the 36 inch diameter reinforced concrete pipe. The reservoir provides 328 acre feet of storage between the normal water level and the crest of the emergency spillway.

4.2 MAINTENANCE OF DAM

The dam is maintained by the owner and is in satisfactory condition. Normal maintenance consists of mowing the bottom of the emergency spillway channels.

4.3 WARNING SYSTEM IN EFFECT

No apparent warning system is present

4.4 EVALUATION

The dam and appurtenant structures are satisfactorily maintained.

SECTION 5: HYDROLOGIC/HYDRAULIC

5.1 DRAINAGE AREA CHARACTERISTICS

Delineation of the watershed draining into the reservoir pool area was made using the USGS 7.5 minute quadrangle for Lisle, N.Y. The watershed consists of woodlands and lightly forested area situated in a rural section. Relief ranges from moderate to steep with the steeper slopes occuring on the western side of the watershed. The slopes on the western side range from 10 to 15%, and on the eastern side they range from 5 to 10%. The oval shaped drainage area is about 1827 acres.

5.2 ANALYSIS CRITERIA

The analysis of the spillway capacity of the dam was performed using the Corps of Engineer's HEC-1 computer program, incorporating the "Snyder Synthetic Unit Hydrograph" method and the "Modified Puls" flood routing procedure. The spillway design flood selected for analysis was the PMF in accordance with recommended guidelines of the U.S. Army Corps of Engineers.

5.3 SPILLWAY CAPACITY

The principal and emergency spillways are uncontrolled structures. The principal spillway operates under weir or orifice flow conditions depending upon the floodwater inflow to the reservoir pool. During orifice flow operation, pressure flow develops in the 36 inch conduit. The emergency spillway was analyzed as a broad-crested weir having a discharge coefficient (C) of 3.087.

The spillways have sufficient capacity for discharging the peak outflow from the PMF. Due to the limited storage capacity, there will be little attenuation of the storm flows. For this storm, the peak inflow and the peak outflow, are both 4905 cfs. When the spillways are discharging the peak outflow, the water surface will be 2.2 feet below the top of the dam.

5.4 RESERVOIR CAPACITY

Normal flood control storage capacity of the reservoir between the principal and emergency spillways is 233 acre-feet which is equivalent to a runoff depth of 1.5 inches over the drainage area. Surcharge storage capacity to the maximum high water elevation is an additional 185 acre-feet; equivalent to a runoff depth over the drainage area of 1.2 inches. Total storage capacity of the dam is 538 acre-feet; equivalent to 3.5 inches of direct runoff.

5.5 FLOODS OF RECORD

The maximum known flood occurred during Huricane Eloise during September, 1975. The pool level at this time was reported to be about 8' feet above the principal spillway crest. The calculated discharge for this flood is as follows:

Elevation (ft) Discharge (cfs)

- 5.6 OVERTOPPING POTENTIAL

 Analysis indicates the total discharge capability is sufficient to prevent overtopping from the PMF.
- 5.7 EVALUATION

 This dam has sufficient capability to impound and adequately discharge floodwaters expected to result from the PMF.

SECTION 6: STRUCTURAL STABILTIY

6.1 EVALUATION OF STRUCTURAL STABILTTY

a. Visual Observations

No signs of major distress of the dam were observed during the inspection.

b. Design and Construction Data

Design data was obtained from the Soil Conservation Service Office in Binghamton. Stability analyses were performed by SCS using a modification of the Swedish Circle Method. The soil parameters assumed for the stability analyses were a friction angle of 31 degrees and a cohesion of 500 pcf. These parameters appear to be appropriate for the type of soil involved. The stability analyses were performed assuming 1 on 3 upstream and 1 on 2.5 downstream slopes with no berms (a berm was used in the final design, but this would increase the safety factor). The results of the analyses are as follows:

CONDITION	UPSTREAM SLOPE	DOWNSTREAM SLOPE
Full Drawdown	2.3	
Long Term Steady State Seepage from Emergency Spillway Crest		2.2

The calculated factors of safety for this dam are in excess of the minimum factors in the Corps of Engineers recommended guidelines. The dam is therefore considered to have an adequate factor of safety for stability.

A summary of the analyses and sections showing the failure arcs are included in Appendix E.

Based on discussions with SCS representatives, the dam was built essentially according to the plans.

c. Post Construction Changes

The SCS representatives were not aware of any changes which have been made on the dam.

d. Seismic Stability

This dam is located in Seismic Zone No. 1. Therefore, a seismic stability analysis is not warranted.

SECTION 7: ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

The Phase 1 Inspection of the Nanticoke Creek Dam No. 9E did not reveal conditions which constitute a hazard to human life or property. The earth embankment is considered to be stable structurally, and capable of safely retarding floodwaters resulting from the PMF.

The design of this dam includes an internal drainage system to control the phreatic surface and to provide a safe outlet for foundation seepage.

b. Adequacy of Information

Information concerning the design and performance of this dam is considered adequate for the purpose required for Phase 1 Inspection Reports.

c. Need for Additional Investigations
No additional investigations are necessary at this time.

7.2 RECOMMENDED MEASURES

The following tasks should be undertaken by maintenance forces:

- a. Periodic operation and lubrication of the mechanically operated slide gate mechanism to insure the ease of operation of the reservoir drain conduit.
- b. A schedule for periodic maintenance should be established which would include items such as mowing the grass on the embankment slopes and crest.

APPENDIX A

PHOTOGRAPHS



RISER - PRINCIPAL SPILLWAY INLET



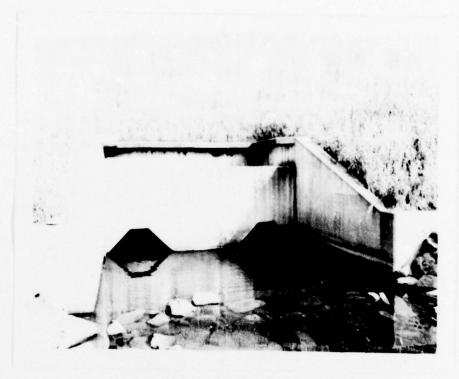
RISER - NOTE LOG LODGED IN TRASH RACK



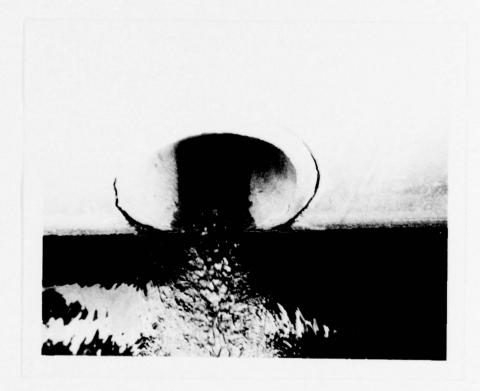
EMERGENCY SPILLWAY LOOKING DOWNSTREAM



DOWNSTREAM SLOPE OF NORTHERN EMBANKMENT



IMPACT BASIN - LOOKING UPSTREAM



OUTLET TO PRINCIPAL SPILLWAY PIPE

APPENDIX B

ENGINEERING DATA CHECKLIST

Engineering Data Design Construction Operation Check List

Name of Dam SITE 9 E

1.D. # N.P. 575 (850 - 3646

			(850 - 3646
Item		Remarks	
	Plans	Details .	Typical Sections
Dam	Y = s	/Es	/ E S
Spillway(s)	٠.6	125	165
Outlet(s)	_ر ر ر) - C	4ES
Design Reports	Yes		
	3		
Design Computations	מיש		
Discharge Rating Curves	•		
Dam Stability	, n		
Sserage Studies	les.		
Subsurface and Esterials Investigations	√es		

Construction History

ONLY INFORMATION AVAILABLE OBTAINED

THROUGH DISCUSSIONS

WITH PROTECT INSPECTOR

Surveys, Modifications, Post-Construction Engineering Studies and Reports

NONE REPORTED

Accidents or Failure of Dam Description, Reports

NONE REPORTED

Operation and Maintenance Records Operation Manual

NONE

APPENDIX C

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1)	Bas	ic Data	
	a.	General	(3)
		Name of Dam NANTICOKE CREEK SITE 9E	
		1.D. # N.Y. 575 (#850-3446)	
		Location: Town NANTICONE County BROOME	
		Stream Name UNNAMED	
		Tributary of NANTICORE CREEK	
		Longitude (W), Latitude (N) W76°3.1' N42°17.5'	
		Hazard Category C	
		Date(s) of Inspection 11/8/78	
		Weather Conditions SUNNY 45°-50°	
	ь.	Inspection Personnel R. WARRENDER : W. LYNICK	
	с.	Persons Contacted H. HIRTH SCS SYRACUSE	
		G. PAGE & D. KOLESAR SCS BROOME CO.	
	d.	History:	
		Date Constructed 1966-67	
		OWNER BROOME COUNTY	
		Designer SCS	
		Constructed by Mc Daugall Const. Co.	9
2)	Tec	chnical Data	0
	Тур	be of Dam EARTH	
	Dra	inage Area SE Acres	
		ight 42 Length South 295	
	line	stream Slone AN 3 Downstream Slone 4N 2.5	

Exter	nal Drains: on Downstream Fa	e	@ :	ownstream	Toe RIP	RAP
Inter	nal Components:					
	Impervious Core					
	Drains 8" CMP DRA	N PIPE IN	SAND E	GRAVEL	DRAIN	,
	Cutoff Type Compact	ED EARTH	FILL			
	Grout Curtain					

	EARTH FILL WITH GOOD VEGETATIVE COVER
3 -	Crest
	(1) Vertical Alignment OKAY
	(2) Horizontal Alignment OKAY
	(3) Surface Cracks NanE
	(4) Miscellancous CREST HAD NOT BEEN MOWED
٠.	Slopes
	(1) Undesirable Growth or Debris, Animal Burrows Scapes HAD
	NOT BEEN MOWED
	(2) Sloughing, Subsidence or Depressions MINOR SLOUGHING ON
	UPSTREAM SLOPE AT WATER SURFACE ELEVATION
	(3) Slope Protection UN MOWED GRASS
	(4) Surface Cracks or Movement at Toe None
	(5) Seepage None
	(6) Condition Around Outlet Structure SATISFACTORY

3)

Abut	tments
(1)	Erosion at Embankment and Abutment Contact None
(2)	Seepage along Contact of Embankment and Abutment None
(2)	Seepage at toe or along downstream face None
Down	FARM FIELDS
(1)	Subsidence, Depressions, etc. None
(2)	Seepage, unusual growth NONE
(3)	Evidence of surface movement beyond embankment toe No Eviden
(4)	Miscellaneous
Drai	inage System

.

Discharge	from Drainage	System	No	DISCHARGE	

Inst	rumentation	
(1)	Monumentation/Surveys N/A	
(2)	Observation Wells N/A	
(3)	WeirsN/A	
(4)	Piezometers N/A	
(5)	Other	
	rvoir	
a.	Slopes FORESTED UP TO WATER'S EDGE	_

10.00

pillwow(s) (including tail race channel)
SATISFACTORY CONDITION
Principle Spillnay 26.2' HIGH RECTANGULAR RC DROP INLET;
BASIN - A 10" DIA LOG WAS LODGED IN THE RISER'S TRACH RA
ALL IN SATISFACTORY CONDITION - VERY SLIGHT SEPARATION AROUND RC PIPE AT JUNICION - WITH IMPACT BASIN HEADWALL -
OPEN CHANNELS IN EARTH CUT.
MOWED BECAUSE OF A LOG LYING IN THE CHANNEL.
Condition of Tail race channel SATISFACTORY
. Stability of Channel side/slopes SATISFACTORY

3)

a.	- ABOVE STREAM BANKS
ь.	Slopes SATISFACTORY - OUTLET INTO WIDE FARM FIELD
c.	Approximate number of homes ABOUT 12-15 IN THE VILLAGE OF NANTICOKE PLUS A CHURCH W/ MEETIN
	House,
Mis	cellaneous

-	uctural .
	Concrete Surfaces SATISFACTORY
	Structural Cracking None
	Movement - Horizontal & Vertical Alignment (Settlement) None
	Junctions with Abutments or Embankments N/A
•	ounce forth with Abdemonts of Embarkments
•	Drains - Foundation, Joint, Face N/A
•	Water passages, conduits, stuices SATISFACTORY
	· · · · · · · · · · · · · · · · · · ·
	Seepage or Leakage None

AT	IMPACT	BASIN -	CONDUIT	GASHA	<u> 7</u> .	_
						_
Foundation						
						_
			···			
Control Gat	es Res	SERVOIR	DRAIN	HAS	SLIDE GATE	-
Annroach &	Outlet Ch	annels				
Energy Diss	ipators (;	plunge poo	1, etc.) <u>/</u>	MPACT	BASIN - OH	A
Energy Diss	ipators (;	plunge poo	1, etc.) <u>/</u>	MPACT	BASIN - OH	A
					BASIN - OH	_
Intake Stru	ctures					
Intake Stru	ctures					
Intake Stru	ctures					

Carlo Santonia

APPENDIX D

HYDROLOGIC/HYDRAULIC

ENGINEERING DATA AND COMPUTATIONS

CHECK LIST FOR DAMS HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

AREA -CAPACITY DATA:

		Elevation (ft.)	Surface Area (acres)	Storage Capacity (acre-ft.)
1)	Top of Dam	1191.8	41.0	_538
2)	Design High Water (Max. Design Pool)	1189.4	37.0	446
3)	Auxiliary Spillway Crest	1186.7	32.2	353
4)	Pool Level with Flashboards	N/A		
5)	Service Spillway Crest	1176.7	16.2	120

DISCHARGES

		(cfs)
1)	Average Daily	N/A
2)	Spillway @ Maximum High Water	165
3)	Spillway @ Design High Water	161
4)	Spillway @ Auxiliary Spillway Crest Elevation	156
5)	Low Level Outlet	14
6)	Total (of all facilities) @ Maximum High Water	11920
7)	Maximum Known Flood	152

CREST:			ELEVATION:	1191.8
Type: LEVEL;	SRASSED EARTH			
Width: 15			NORTH SECTION	295
Spillover N/A				
Location				
SPILLWAY:				
PRINCIPAL			EMERGE	NCY
1176.7	Elevation	on	1186.7	
RC DROP INLET W/TR	ASH RACK Type	2 7	RAPEZOID	AL CHANNELS
3'x9'	Width	EACH	150' WITH	lon 3 SLOPES
	Type of Contr	rol_		
✓	Uncontrolle			
	Controlled	i :		
N/A	Туре		N/A	
	(Flashboards; ga		•	
N/A	Number		NIA	
N/A	Size/Length	1	N/A	
	Invert Materia	Mau Mau	ED GRAS	5
	Anticipated Ler of operating ser	ngth rvice _	< PER	100 Yes
BG" DIA RC ZOS FT	Chute Length	NORTH	4501 5	OUTH 750'
SHARP (RESTED	deight Between Spi	llway Cre	est N/A	
L/6=1.0	& Approach Channe (Weir Flow	al Invert	BROAD	CRESTED WELL
Ware / aug 7 + = 12/	(

CUTLET STRUCTURES/EMERGENCY DRAWDOWN FACILITIES:- RESERVOIR DRAW
Type: Gate V Sluice Conduit V Penstock
Shape: GATE- FLAT CIRCULAR CONDUIT - ROUND CAST / RON
Size:
Elevations: Entrance Invert 1153.0
Exit Invert 1144,5
Tailrace Channel: Elevation 1144.5
HYDROMETEROLOGICAL GAGES:
Type: NONE
Location:
Records:
Date -
Max. Reading -
FLOOD WATER CONTROL SYSTEM:
Warning System: None
Method of Controlled Releases (mechanisms):
NONE EXCEPT FOR MANUALLY OPERATED RESERVOIR
DRAIN SLIDE GATE

INAGE AREA:	1827 ACR	53	7 86 SQ N	1/	
INAGE BASIN RUNOFF (CHARACTERISTIC	۲.			
Land Use - Type:					
Terrain - Relief:	MODERATE -	STEEP			
Surface - Soil:	GLACIAL	TILL			
Runoff Potential (existing or pl surface or sub			s to existing	
N _c	ONE				
Potential Sedimenta	ation problem	areas (natura	l or man-made:	present or f	-,,+,,
					2 6 6
		areas (natura			464
No.		areas (macara			
					_
		areas (macara			
No.	y E	s for levels		orage capacity	_
Potential Backwater including sur	r problem area	s for levels	at màximum sto		_
No.	r problem area	s for levels			_
Potential Backwater including sur	r problem area	s for levels	at màximum sto		_
Potential Backwater including sur	r problem area	s for levels	at màximum sto		_
Potential Backwater including sur	r problem area rcharge storag	s for levels	at màximum sto		_
Potential Backwater including sur None	r problem area rcharge storag	s for levels	at maximum sto		_
Potential Backwater including sur None	r problem area rcharge storag	s for levels e: on-overflow)	at maximum sto		_
Potential Backwater including sur None	r problem area rcharge storag	s for levels e: on-overflow)	at maximum sto		_
Potential Backwater including sur None None Dikes - Floodwalls Reservoir per Location:	r problem area rcharge storag	s for levels e: on-overflow)	at maximum sto		

MANTICOKE DAM SITE #9E

D.A. = Drainage area in square miles L = River mileage from the given station to the upstream limits of the drainage area LCA = River mileage from the station to the center of gravity of the drainage wea PMP = Probable Maximum Precipitation in inches to = Lag time from mid-point of unit rainfall duration, to, to peak of unit hydrograph, in hours. to = Unit rainfall duration, equal to to in hours. Ct = Coefficient depending upon units and dramage basin characteristics ta = unit rainfall duration other than standard unit; tr. adopted in specific study, in hours tope = lag time from mid-point of unit reminfall duration, ER, to peak of unit hydrograph, in hours D. A = 2.86 square miles, L = 3.07 miles, La = 1.40 miles Pmp = 20.5 inches C4 = 2.0 Cp = 0.625 from average 640 Cp = 400 tp = Ct (L. Lca)0.3 = 2.0 ((3.33)(1.32)]. 3.10 hours tr = to = 3.10 = .56 hours (use I hr. hydrograph) tpR = tp +0.25 (te - tr) = 310 + .25 (1-.58) = 3.21 kms. From HMR 33 - Figure Z , Deplk - trea - Duration 6 hour % 111 = 12 hour 1/4 = 133

. 48 hour % = 142

2 A hour % 172 =

PROJECT GRID

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HEC-1 VERSION DATED JAN 1973 UPDATED AUG 74

DATE MULTI-PLAN ANALYSES TO BE PERFORMED NPLAN 1 NRTIO= 2 LRTIO= 1

0.50 RT105=

******** ******* *** *** ***

JPRT INAME SUB-AREA RUNDFF COMPUTATION ISTAQ ICOMP IECON ITAPE JPLT 0 0 0 0 0

LOCAL RATIO ISNUM ISAME HYDRUGRAPH DATA TRSDA TRSPC 2.86 0. SNAP 0. IUHG TAREA 1HYDG

SPFE PMS R6 R12 R24 R48 0. 20.30 111.00 122.00 133.00 142.00

TP= 3.00 CP=0.63 NTA=

RTIND 0.

ALSHX 0.

ERAIN STRKS RTICK STRTL CNSTL

STRKR DLTKR RTIDL

UNIT HYDROGRAPH 15 END-OF-PERIOD ORDINATES, LAG. 2.98 HOURS, CP. 0.63 VOL. 1.00
216. 357. 374. 284. 188. 124. 82. 54. RECESSION DATA
STRTQ# 4.00 QRCSN# 4.00 RTIDR# 1.00
APPADXIMATE CLARK COEFFICIENTS FROM GIVEN SHYDER CP AND TP ARE TC# 3.71 AND R# 2.44 INTERVALS

36.

END-OF-PERIOD FLOW 00000000 TIME

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PEAK FLOW SUNMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS

RATIOS APPLIED TO FLOWS		
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0.50	2452.	2527.
PLAN	~	7 - 7
STATION	1 1	•
OPERATION	HYDROGRAPH AT	ROUTED TO

APPENDIX E
STABILITY ANALYSES

2 -- W. S. Atkinson -- 5/25/65

Rey S. Decker

Subj: ENG 22-5, New York WP-08, Nanticoke Creek, Site No. 9-E

(Broome County)

EMBANKMENT

- A. Classification: Embankment samples are classified GM and GC based on the gradation that includes 20% plus 3-in. material. Actually, the laboratory samples, 65W2924 and 65W2925, contained slightly over 50% fines.
- B. Density: Standard moisture-density tests were made in the minus 3/4-in. fraction. Maximum density ranges from 124.5 to 126.5 p.c.f.
- C. Shear Strength: Sample No. 65W2925 was tested, using the minus 3/4-in. fraction. One hundred percent of standard density was selected because previously tested similar material had relatively low shear strength at lower densities.

Shear values from this CU test are $\emptyset = 31^{\circ}$, c = 500 p.s.f. Effective stress parameters are $\overline{\emptyset} = 32.5^{\circ}$, $\overline{c} = 550$ p.s.f., correcting for measured pore pressure.

SLOPE STABILITY ANALYSIS

An embankment only analysis using laboratory charts based on a modification of the Swedish circle method and using shear values of $\emptyset = 31^{\circ}$, c = 500 p.s.f. indicates that the factor of safety of a 3:1 upstream slope and 2 1/2:1 downstream slope is in the range of 2.0. Drawdown to the base is assumed and the phreatic surface is assumed to emerge on the downstream slope.

It is concluded that more detailed analysis is not justified.

CONCLUSIONS AND RECOMMENDATIONS

- A. Site Preparation: It is recommended that the soft surface silts be removed. Most of this soil will be taken out in normal stripping operations.
- B. Centerline Cutoff: Cutoff of disturbed surface soil is recommended for the abutments. Cutoff of the alluvial gravels into till is recommended for the floodplain area. A 25-foot bottom width is recommended for this cutoff to reduce the exit gradient into the alluvial gravels. The GC material is satisfactory for backfill.
- C. Principal Spillway: No particular problems are anticipated.
- D. Drainage: With the proposed cutoff, the alluvial gravels downstream are expected to function as a drain. You may wish to consider a pick-up trench drain or a small rock toe to outlet this natural drain.

3 -- W. S. Atkinson - 5/25/65

Rey S. Decker

Subj: ENG 22-5, New York WP-08, Nanticoke Creek, Site No. 9-E (Broome County)

E. Embankment Design:

1. Selection of Material. Material like sample Nos. 65W2924 and 65W2925, GC and GM, can be used anywhere in the embankment. It is suggested that consideration be given to placing the coarser gravel with low-plastic fines, 65W2926 - GM, in the downstream base section provided it is practical to separate it from the other soils. Permeability of this material is expected to be somewhat higher than that of the others.

The recommended density control is 100% of standard based on the minus 3/4-in. fraction. Shear strength at this density is ample based on the test for Sample No. 65W2925. Notify us if you prefer a lower control than 100% of standard and another shear test and slope stability analysis will be made.

- 2. Slopes. Proposed 3:1 upstream and 2 1/2:1 downstream slopes are . adequate.
- 3. Settlement Allowance. An allowance of 1.0 ft. is suggested to compensate for residual settlement in embankment and foundation; 0.8 ft., 2% average, for the embankment and 0.2 ft. for the foundation.

Robert E. Nelson

Reviewed and Approved by:

Roland B. Phillips

Attachments

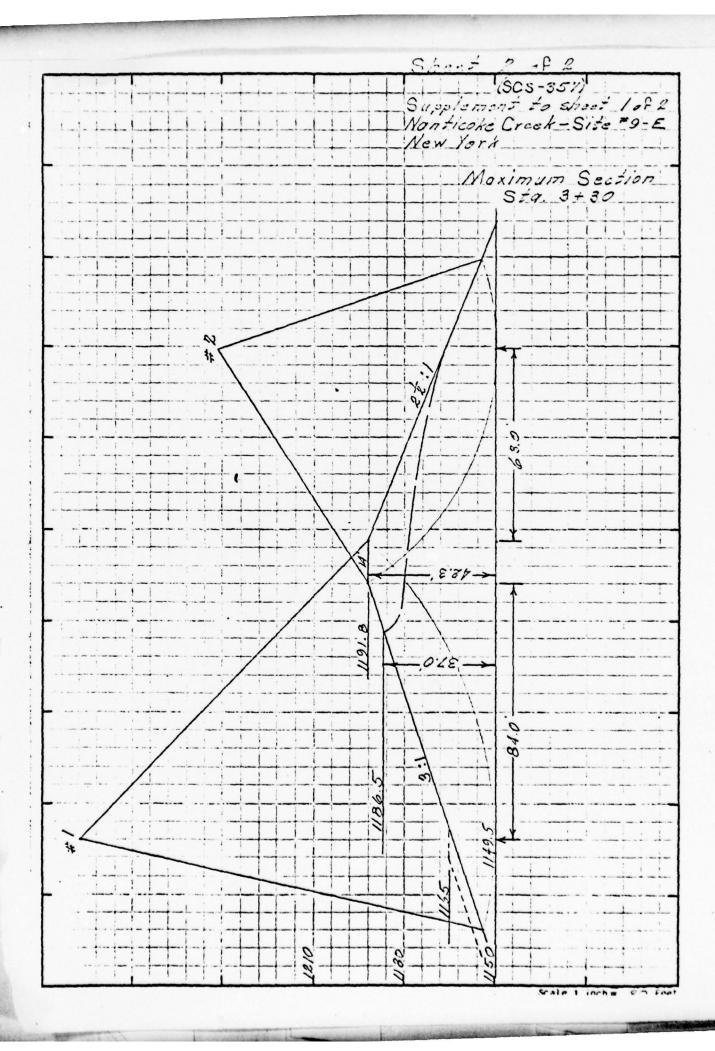
cc: B. S. Ellis, Syracuse, New York
Henry W. Davis, Penn Yan, New York
R. J. McClimans, Binghamton, New York
H. M. Kautz, Upper Darby, Pennsylvania

FORM SCS-357 10-58

U. S. DEPARTMENT OF AGRICULTURE Maximum Section

SOIL MECHANICS LABORATORY

SUMMARY - SLOPE STABILITY ANALYSIS												
State May York Project MaiTICORE CREEK-SITE 9-6											9-5	
				_ Analys						y		
Method o	f Anal	ysi	s		WE	2/54	Cu	PCA.F				
Locati	on						5/2:	, ",				
of	,						95 % M	Sta				
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7 d								24.7			-	
7 m							137.0					
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7 5								3.0				
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APPENDIX F

REFERENCES

APPENDIX F

REFERENCES

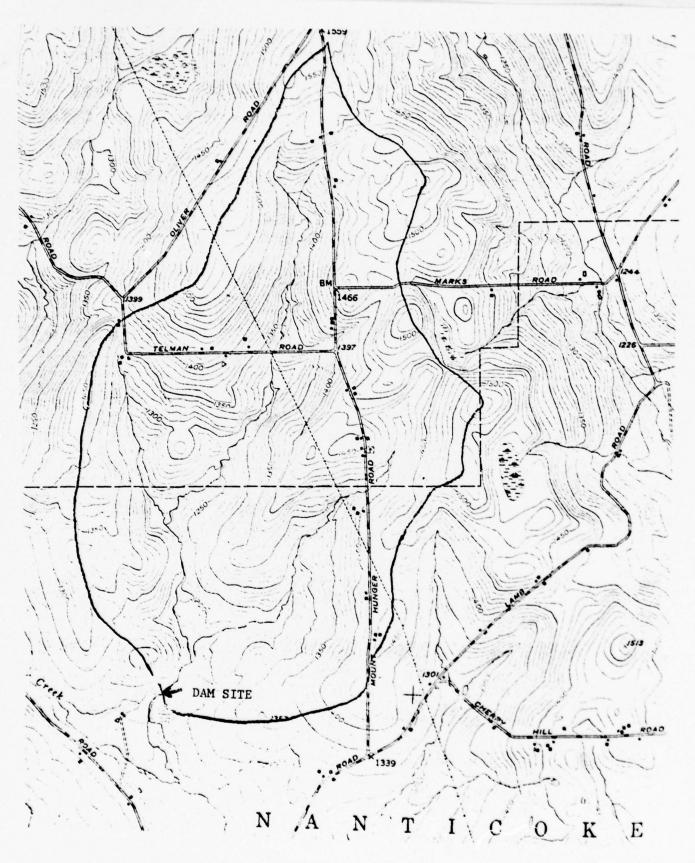
- 1) U.S. Department of Commerce, <u>Technical Paper No. 40</u>, Rainfall Frequency Atlas of the United States, May 1961.
- 2) H.W. King and E.F. Brater, <u>Handbook of Hydraulics</u>, 5th edition, McGraw-Hill, 1963.
- University of the State of New York, Geology of New York, Education Leaflet 20, Reprinted 1973.
- 4) Elwyn E. Seelye, Design, 3rd edition, John Wiley and Sons, Inc., 1960

APPENDIX G

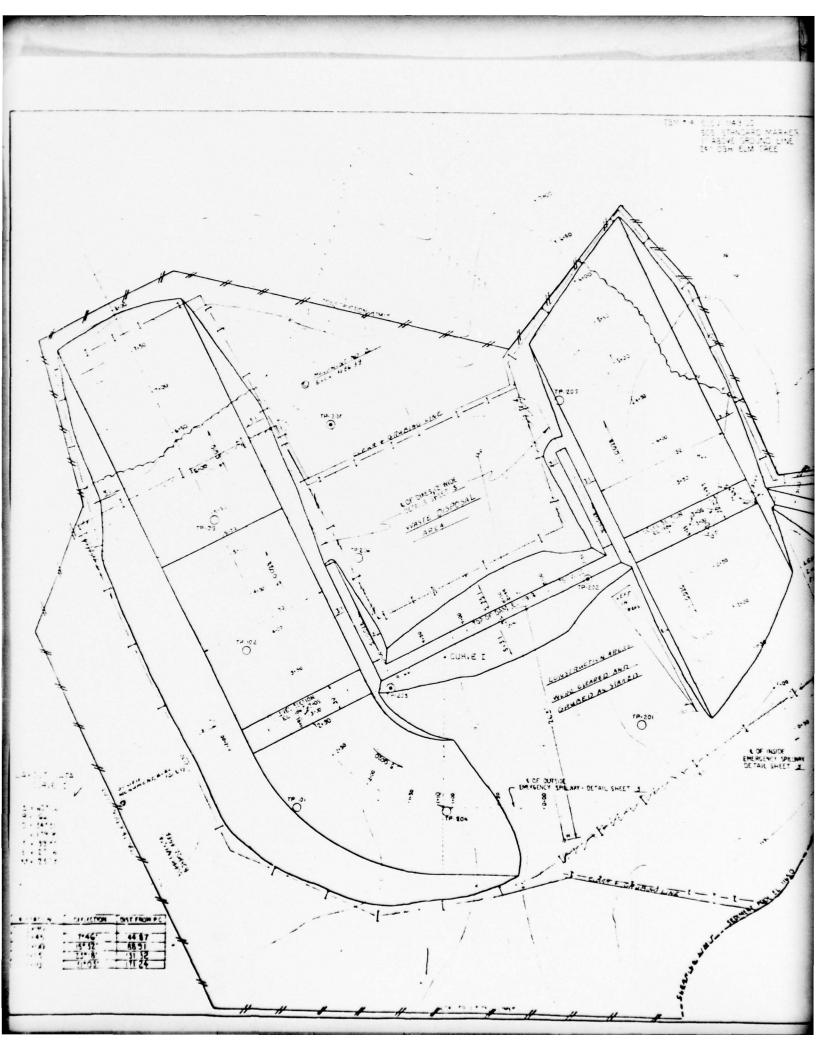
DRAWINGS

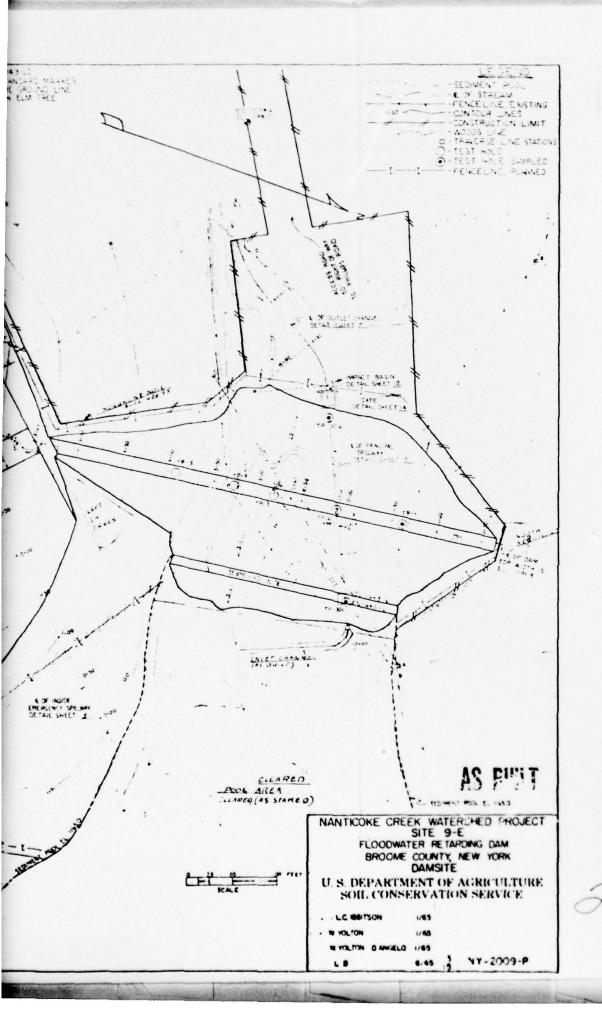


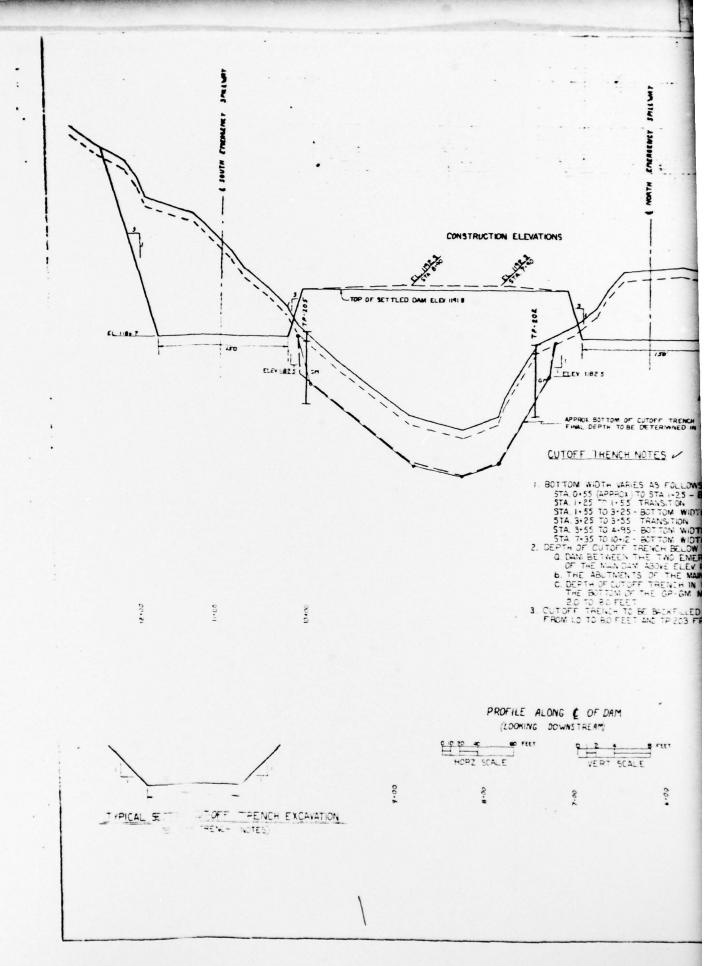
NANTICOKE CREEK WATERSHED PROTECTION PROJECT DAM SITE No. 9E

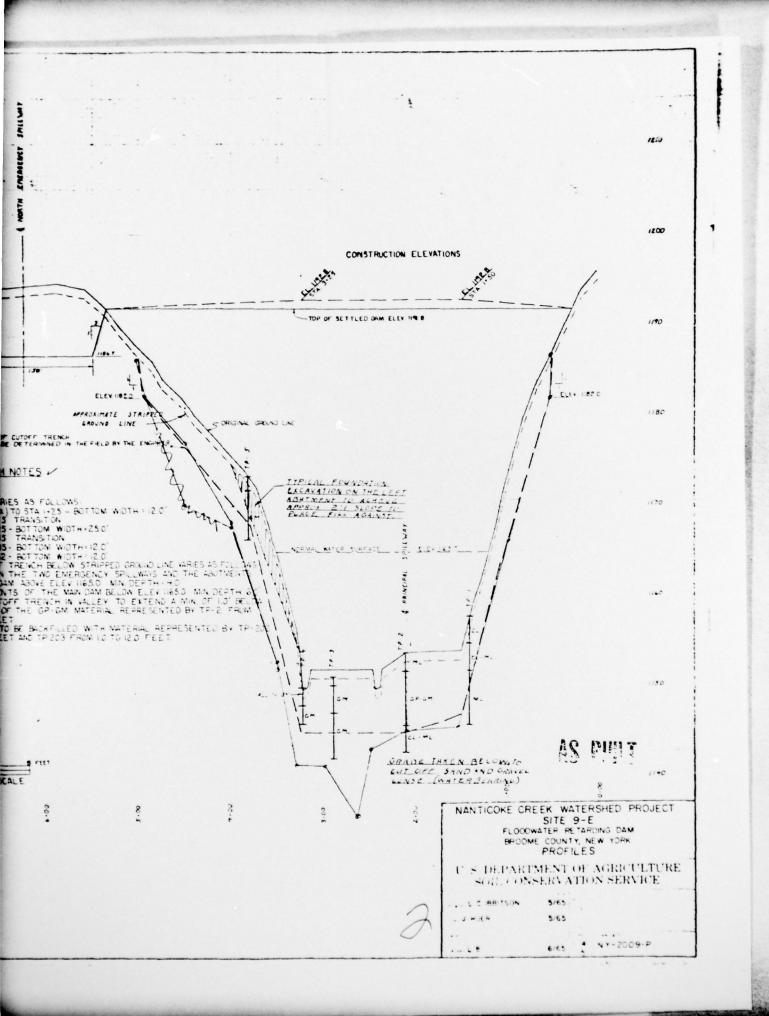


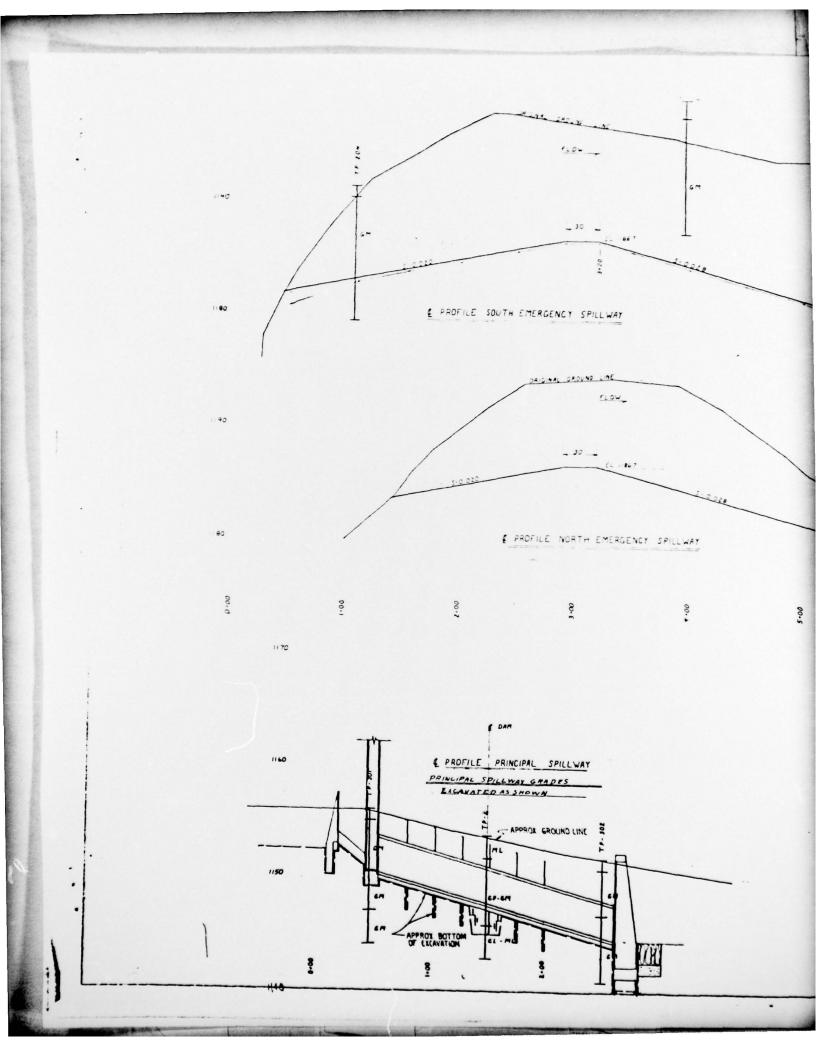
TOPOGRAPHIC MAP
NANTICOKE CREEK WATERSHED PROTECTION PROJECT
DAM SITE No. 9E

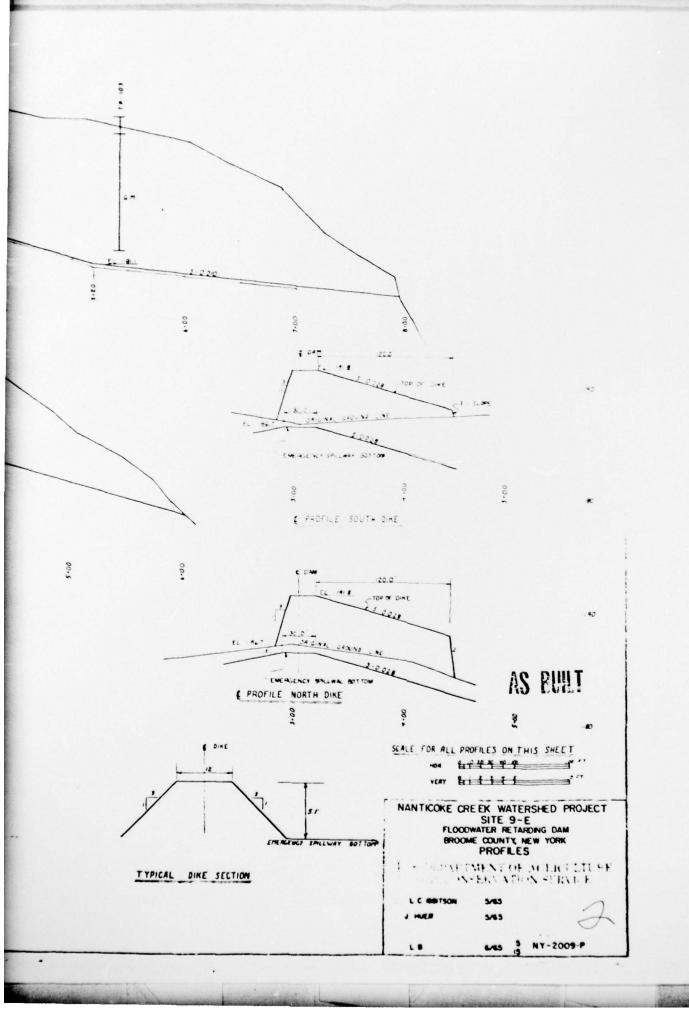


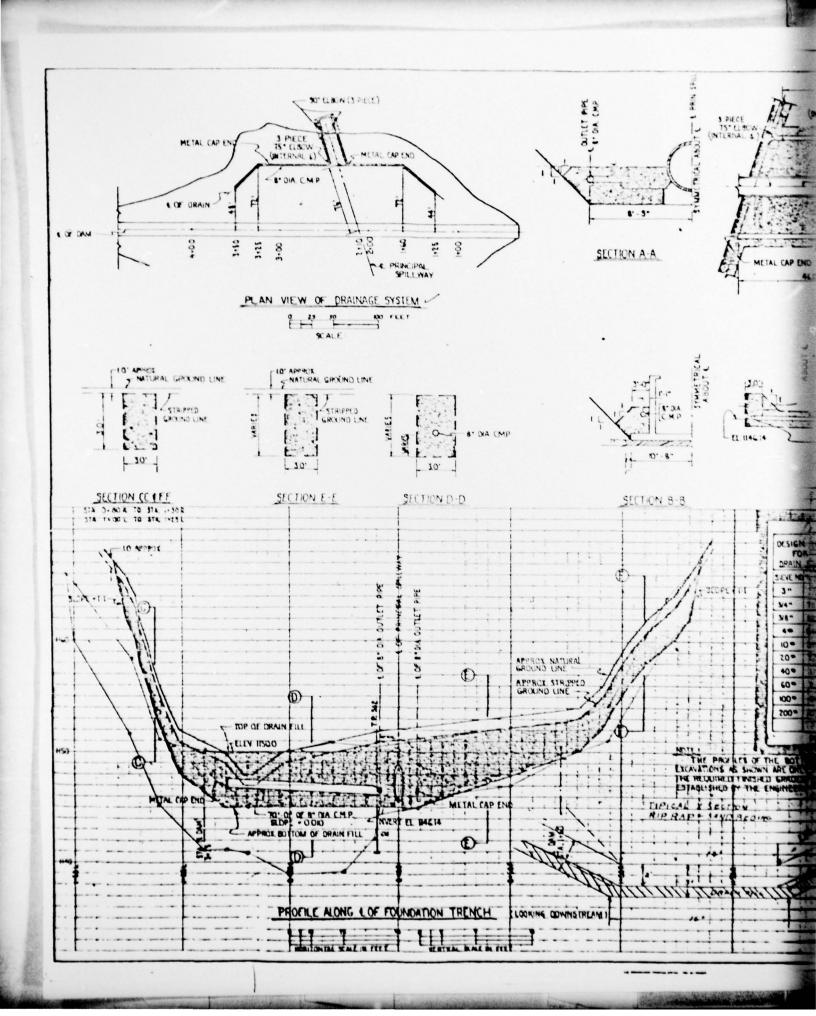


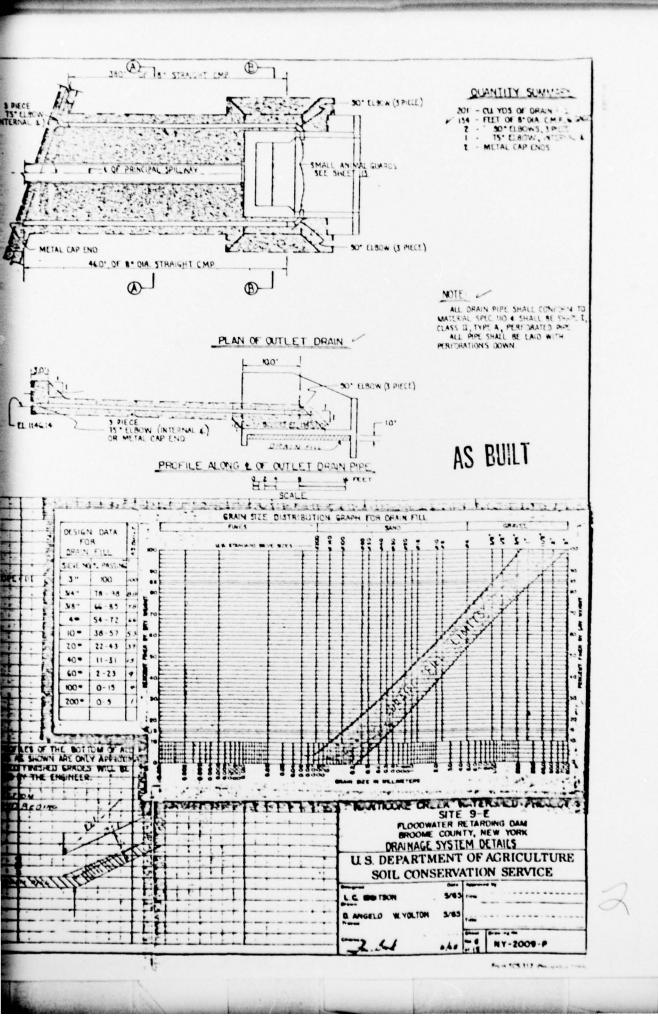






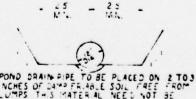






3/16 40. 3/10 80 -7. 90 120 180. DET_ET 206 13 _ < 4% | SEEF 12 LANS REINE 2010 10455 40 CETALS 1-EET_0 449 IF TI PROFILE ALONG & OF PRINCIPAL SPILLWAY 1115. 3 E 1 1 1 -

TYPICAL SECTION-INLET CHANNEL



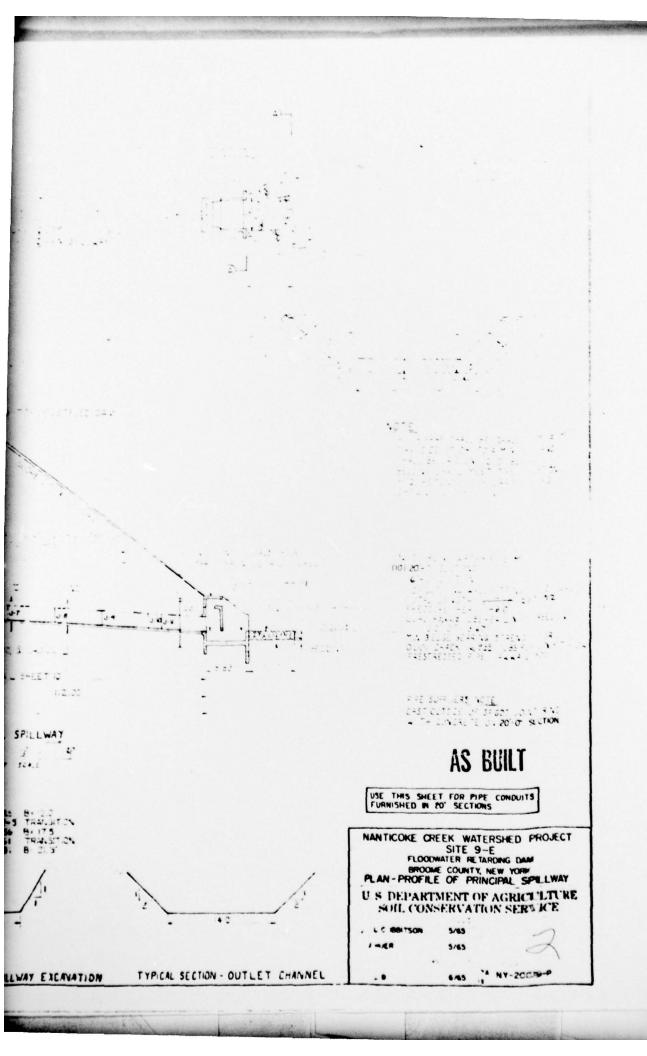
POND DRAIN PIPE TO BE PLACED ON 2 TO 3
INCHES OF DAMP FR. ABLE SOIL FREE FROM
LUMPS THIS MATERIAL NEED NOT BE
COMPACTED BEFORE PLACING THE FRE
BUT MUST BE GRAVED TO 4 TRUE PLANE

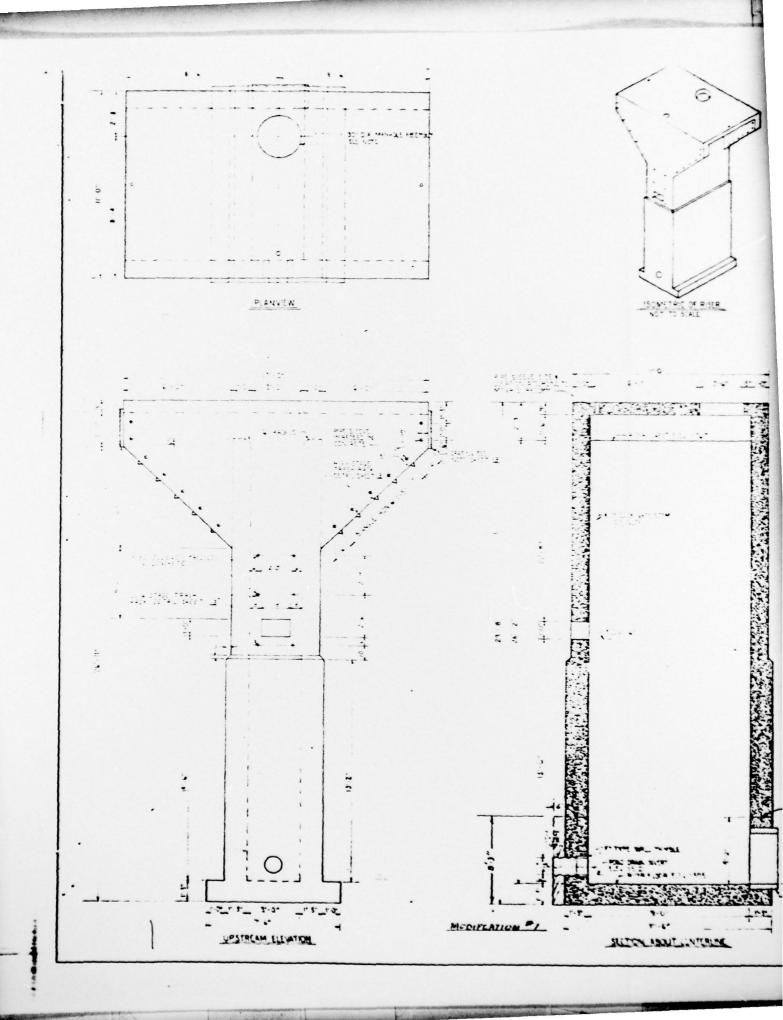
TYPICAL SECTION - POND DRAIN EXCAVATION

8

STA 3-44 T. STA 2-92 B. 23 STA 2-35 TO STA 2-3-5 TRAUJE STA 2-2-5 TO STA 2-56 B. 175 STA 2-5-5 TO STA 2-61 TRAUST STA 2-61 TO STA 2-81 B. 21.5

TYPICAL SECTION - PRINCIPAL SPILLWAY EXCANATI

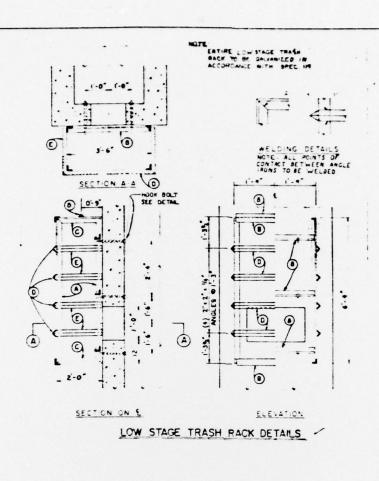




MAN-DE ASSING - NOTES

/ SO DA MANHOLE WITH UNDERSIDE -DORS
AND A FOLAMIA ROUND -DLE LIFTING DEWICE
2 PAINT IN ACCORDANCE WITH CONST SPECIAL - . SLOS DATE NOTES **. STRUCTURAL CARBLA STEEL PLATE GAZETO I E DIA FLAT FRAME SLIDE GATE
2 WOBES AND WEDGE SEATS SHALL BE SHINT
3 SEATING MEAD OF
4 OPERATING MEAD LAD
5 UNSCATING MEAD LAD
5 UNSCATING MEAD LAD
6 TO THE WALL THIMBLE DOES MEDICE TO
7 TO STUB OF TO DIA/G SASE TIME
1 RISING STEM, THEADLE BOSTON BROWLE
8 STEM, STEM SAJES, AND UTFING DELIE TO
AND SPACID ACCORDING TO MANUFACTURES
RECOMMENDATIONS
9 PAINT IN ALCORDANCE WITH LONG SPECIAL
FANTAMED - BLOWN, MEAN. STEE PLATE IN WALLS TO BE CONTINUOUS AROUND RISER IDIN'T TO BE WELDED OR BOLTED. V4. L. STRUCTURAL CARBON STEEL PLATE GRACETO INSTALLED - RECNET HAT MEDEL 185 PLATE CONST JOINT DETAILS AN Sharp To Day on HHE I LI I I VZ Bint NAT CAR. YEA. NANTICOKE CREEK WATERSHED PROJECT SITE 9-E FLOODWATER RETARDING DAM BROOME COUNTY NEW YORK RISER DETAILS U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE SMEDT SAFE TO 243 . WP YOL TON RINK DOWNS THEAV ILL ATION 9 NY- 2009-P

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HOOK BOLT DETAIL GALL IPST. SUPPLY WINUTE & AMS-ERS

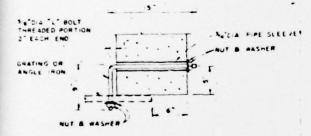
. - 10 SEE DETAIL ANGLE IRON (A) ANGLE IRON (A) STEEL STRAP DETAIL 6 REO'D. SCE DETAIL NOTE-ENTIRE HIGH STAGE TRASH RAIR TO BE GALVANIZED IN ACCORDANCE WITH SPEC. 119 STEEL STRAP N' . M' STEEL BEARMS & GRATINE HIGH STAGE TRASH RACK DETAILS

THREADED P

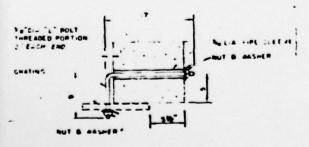
GRATING OR

	BILL OF MAT	ERIAL .	1.	
-00A-104	178 4	SZE	LENGT-	3-44
LOW STACE	B MAGLE FOR	22.74.0	64	
YRA ME MEN	MIGLE INCH	27.22.4	J- 50	
	C MIGLE INDIN	28 . 28 . 4	2-0	
	D MAGLE MON	12.5.0	5.10	
	D MIGLE MON	18.2.5	Z . W	
	HOOK BOLT MAUTS AND WASHERS	14 OM .	-	
	DOL STIENE	44 DIA	1-0	
HIGH STEE	& MIGLE MON	1.5.5	0-0	
TAASH RACK	L SOLT ME : "NUTS AND WASHERS	40 DIA	9. 5	20
	L BOLT WE E MUTS AND WASHERS	. Se DIA	9.17	1
	MEG NEE BOLT YMUTS MO WASHERS	YE' DA	0-19	1
	PIPE SEEME	Nº DIA	1.0	2.0
	PIPE MEENE	M OHA .		1
	STEEL STRAP	2.14	2-5	
1	CRATING	27.0.0		

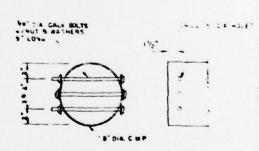
"NA" DIA PIPE SEETSE



BOLT DETAIL Nº 1



BOLT DETAIL Nº 2



SMALL ANIMAL GUARD DETAILS /

AS BUILT

NANTICOKE CREEK WATERSHED PROJECT

SITE 9-E

FLOODWATER RETARDING DAM

BROOME COUNTY, NEW YORK

TRASH RACKS AND MISC DETAILS

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

LC BUTSON 4-6002-AN B . 1279



2 4 1 to 110

- I deprise and rate, and off not now are training out of normal permanent or permanent of the rest of t
- of the state of th

2, CA, Qcv. 1151.4

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>

2

3

- 0 2 Tupori, silt and fine or need Recent Alimons - light prove or sat - Slowuble - Recent - suit to education
- The Gravel, about 10% fines subcorded coarse fraction brow set to bate from mud. percentle peobably Recent Allered dense.

 D.S. 2.1 moved 66774
- H II Clay, sulty shore but -200 graying thrown set very should personable first till phase very should (L.L.-24, F.I.-- 0.5. 2.5)

T 3, CA, Ejer, 1151.2

- e 1 faranti
- 1 4 Gravel, well graded down to about 19% files—20) charse fraction solved at tabular and manufacture brown set to saturated at 3.5% coderately personable probable Recomt alluvium mod. loose (seepage at 3.5%).
- 4 9 Gravel, approximately 10% +3" and 40% (unexp-10%) fairly well graded - 2ray - moist to out slowly personale - Bingrawton drift (zlacual till) - very dende.

T 4 CA. Elev. 1150.0

- 0 2 Rece t Min.w, stress ravel and fl & se rus.
- 2 4 Oravel, approximately 10% +3% and 40% filtered CM) facility well crusted - gray - noise to wet slowly per early - Bingulator fruit (placus) till) - very dense.
 - NOTE: Grades into brownsh ciscual till in te ---

7 5, C1, Eler. 1173.3

- 0 1.5 Treseil
- 1.5 7 Gravel, approximately 20% ed" and 40% filmes—(20) fairly will graded brown moist to wet slowly perceable Bingmacton drift (/lacial till) very dense.

17 101, B.rrev, Elev. 1203.4

- e 1 fishil
- i 11 Gravel, approximately 20% -19 and 40% pares-(20) a new en-10 blooky consider - fairly smill predict - Prow - moust to vet - showly personalse - Bing meters trace (gracial till) -

77 102, 8 rraw, Eles, 1199,4

- C 1.5 Topseil
- 1.5 12 Gravel, approximately 15 +1" and 45 fixes(OR) fairly will graded = in white mounts to wet a slowly permeable = 81 to instant drift (placial till) = very dense.

W 103, Berrie, fler. 11-4.2

- C 1.5 forecil
- 1.5 12 Gravel, approximately 205 +3" and 405 fines(OH) fixely will creded leads moist to wet slowly permeable Bingramtum drift (glacial cill) very dense.

W 201, Lar, Seill., Cler, 11-1.4

- O 1 Topocil
- 1 12 Gravel, approximately 20% +3" and 40% fines(Ch) fairly well graded - brown - mist to set alowly personals - Binehouses drift (glacial till) - very dense.

. B 202, Lor. Saill., Eler. 1179.0

e 1 Topos Li

-

Gravel, apprenently 205 +9" and 405 fines (On) fairly wall graded - recur - mist to vet - CL slowly permode - Displacement of tift (glacial till) - very dense, 8.6, 202.1

7 31 Let 2 1 1 Let 11-1 .

- e i Lieu
 - if or it, spor knowing NM M and and times (AN)
 facility will raise from a set to wet times per mode Rose arts trust Classal
 till term areas.

If AN Let Spills Blow street

- C 1 Tym-1
- 1 12 Or well, approximately 20% *** _ 2 ac% fines(20) locals of our local plants well, graded a rose small to set shally presented standards trust (section till) er, dense

W 105, East. St. L. Lie, Let. 1

- e i fore di
- General, approximately (ob -)* and tot fineside)
 in-106 volumes fairs, well readed God
 from what to wet sinch permeable Sing among fruit (gracial till) very dense.

 D.S. 205.1

Tr : De, Eler. St ... Elen. 114.4

- 0 1 Topsoil
- 1 "Oracel, approximately 25 -3" and 405 fines(DE) 10-125 -0" unders - fairly cell graded brown - moist to cet - al-aly personable -Bluggardon drift (placeal vill) - very dense.

7 W. Ler. Spill. Her. Uno.s

- 0 1 Topecil
- 1 II Gravel, well grated, with approximately (OH) 20% +9° and occasional rim cobrlex about GM 40% fixes broad resist to set slowly permeasus Bing across drift (placeal till) serv de se (a somewhat pire bilty sand toos mas en functored at the 7°l level probably not extensive). D S. 207.1

P K1, Pr. .. Spill., Elev. 1150.1

- e 1 Topeosl
- 1 5.5 Gravel, well mained down to about 155 (GN)
 files course fraction assemble tracillar
 and a rain lar cross set to sat at 3.57 motionities permattle protectly Recomt
 alloyane wed, loose (seepage at 3.57).
- 5.5 9.0 Gravel well graded down to 20% fines (ON) trown do se (increasing downty widepth) wid. perm. sat rated (atony till).
- 9 12 Oracel, approximately 20% +1" and 40% ON face fairly well graded gravist brown wrist to wet slocky personnle Singulation iniff (placed till) very dense.

 D.S. 301.1

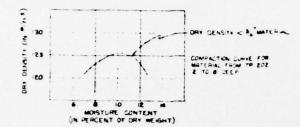
7 102 Prus. Spill , Elev. 1151."

- 0 1 T ps. 1
- 5 Gravel, well ground down to about 19% Getines coupse fraction s new at tocular and submurcilar brown wet to sat, at 3.5' waterutely permeable probably Recent all name wad, loose (accepage at 3.5').

 D.S. 302.1.
- 5 II Gravel, approximately 20% +3" and 40% (GN) fuses - fairly well graded - gray - moist to wet - slowly permeable - Singlement drift (glacual till) - very dense.

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COMPACTION CURVES



-24

ORY DENSITY < % WITE MAN. COMPACTION CURIE FEED INSTEAD FOR DEEP MOISTURE CONTENT (IN PERCENT OF DRY WEIGHT)

Test sale Valerty meter

te terme of the			
form are	1.1	-	
ALIECA & TIED		-	
enterior of metler atrict or	W. 2		-
tres ca el			-
elier -lia	4.1	*	•

SIFE SHE CASSIFICATION STEP SENDE

OH salty gravele; previously state electrons
ML State; sulty, v. function design and v. of the marks
SH sales, sulty
Georges, clean, well graded
CL Chars - t. liquid limit of 50 or less
Of Fourity graded gravels

SAMPLE

as Pist red

- All s il alt no rescriptio s alt chicarications were determined by the all execution.
- (F.X.) UNIFED CLASSIFICATION MADE BY VISUAL INSPECTION IN FIELD
- X X UNIFED CLASSIFICATION BY LABORATORY

AS BUILT

NANTICOKE CREEK WATERSHED SITE-9E

LOGS OF TEST HOLES

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

SOIL CONSERVATION SERVICE

